# 3A, Full Featured DC/DC Converter with Soft-Start and Inrush Current Protection 

## feATURES

- Wide Input Voltage Range: 2.5 V to 24 V
- 3A, 42V Internal Switch
- High Efficiency Power Conversion: Up to 89\%
- Soft-Start
- Frequency Set by External Resistor: 200kHz to 3.5 MHz
- Protection Against Input Short Circuits and Hot Plugging
- Low $\mathrm{V}_{\text {CESAT }}$ Switch: 0.3 V at 2.5 A (Typical)
- Capable of Positive and Negative Outputs
- Available in Thermally Enhanced 14-Lead (4mm $\times 3 \mathrm{~mm}$ ) DFN and 16-Lead TSSOP Packages


## APPLICATIONS

- High Power LED Driver
- DSL Modems
- Distributed Power


## DESCRIPTIOn

The $\mathrm{LT}^{『} 3479$ is a current mode, fixed frequency step-up DC/DC converter with an internal $3 \mathrm{~A}, 42 \mathrm{~V}$ switch. Efficiencies of up to $89 \%$ can be achieved in typical applications. It features a programmable soft-start function to limit inductor current during start-up and inrush current protection to protect the LT3479 during shorts and line transients. Both inputs of the error amplifier are available to the user allowing positive and negative output voltages. Through an external resistor, the user can program the switching frequency from 200 kHz to 3.5 MHz . The low profile ( 0.75 mm ) 14 -pin, $4 \mathrm{~mm} \times 3 \mathrm{~mm}$ DFN package provides excellent thermal performance in a small footprint. The LT3479 is also available in a thermally enhanced 16-pin TSSOP package.

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## TYPICAL APPLICATION

5V to 12V Boost Converter


5V to 12V Efficiency


# ABSOLUTE MAXIMUM RATINGS <br> (Note 1) 

## SW, L, V V Voltages <br> $\qquad$ <br> $V_{I N}$, SHDN Voltages <br> $\qquad$ <br> FBP, FBN, $\mathrm{V}_{\text {REF }}, \mathrm{R}_{\mathrm{T}}, \mathrm{V}_{\mathrm{C}}$ Voltages ........................... 2 V <br> Junction Temperature ....................................... $125^{\circ} \mathrm{C}$ <br> PACKAGE/ORDER INFORMATION

Operating Temperature Range (Note 2) .. $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ Storage Temperature Range ................ $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ Lead Temperature (Soldering, 10 sec ) TSSOP $300^{\circ} \mathrm{C}$


Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS
The $\bullet$ indicates specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. $\mathrm{V}_{I N}=2.5 \mathrm{~V}, \mathrm{~V}_{\overline{\text { SHDN }}}=2.5 \mathrm{~V}$.

| PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Input Voltage |  | $\bullet$ |  | 2.3 | 2.5 | V |
| Quiescent Current | $\begin{aligned} & V_{I N}=2.5 \mathrm{~V}, \mathrm{~V}_{\overline{\text { SHDN }}}=0 \mathrm{~V} \\ & \mathrm{~V}_{I N}=2.5 \mathrm{~V}, \mathrm{~V}_{\text {SHDN }}=2.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.3 \mathrm{~V} \text { (Not Switching) } \end{aligned}$ |  |  | $\begin{gathered} 0.1 \\ 5 \end{gathered}$ | $\begin{gathered} 1 \\ 7.5 \end{gathered}$ | $\mu A$ $m A$ |
| Reference Voltage | Measured at $\mathrm{V}_{\text {REF }}$ Pin | $\bullet$ | 1.216 | 1.235 | 1.250 | V |
| Reference Voltage Line Regulation | $2.5 \mathrm{~V}<\mathrm{V}_{\text {IN }}<24 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.3 \mathrm{~V}$ |  |  | 0.01 | 0.03 | \%/V |
| Maximum V ${ }_{\text {REF }}$ Pin Current | Out of Pin |  |  |  | 100 | $\mu \mathrm{A}$ |
| Soft-Start Pin Current | SS = 0.5V, Out of Pin |  |  | 9 |  | $\mu \mathrm{A}$ |
| FBP Pin Bias Current |  |  |  | 25 | 100 | nA |
| FBN Pin Bias Current |  |  |  | 25 | 100 | nA |
| Feedback Amplifier Offset Voltage | $F B P-F B N, V_{C}=1 V$ |  | -2 | 2 | 6 | mV |
| Feedback Amplifier Voltage Gain |  |  |  | 250 |  | V/V |
| Feedback Amplifier Transconductance |  |  |  | 150 |  | $\mu \mathrm{S}$ |
| Feedback Amplifier Sink Current | $\mathrm{V}_{\text {FBP }}=1.25 \mathrm{~V}, \mathrm{~V}_{\text {FBN }}=1.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.5 \mathrm{~V}$ |  |  | 10 |  | $\mu \mathrm{A}$ |
| Feedback Amplifier Source Current | $V_{\text {FBP }}=1.25 \mathrm{~V}, \mathrm{~V}_{\text {FBN }}=1 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.5 \mathrm{~V}$ |  |  | 10 |  | $\mu \mathrm{A}$ |
| Switching Frequency | $\begin{aligned} & \hline \mathrm{R}_{\mathrm{T}}=17.8 \mathrm{k} \\ & \mathrm{R}_{\mathrm{T}}=113 \mathrm{k} \\ & \mathrm{R}_{\mathrm{T}}=1.78 \mathrm{k} \end{aligned}$ |  | $\begin{gathered} 0.9 \\ 160 \\ 2.7 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1 \\ 200 \\ 3.5 \\ \hline \end{gathered}$ | $\begin{aligned} & 1.15 \\ & 240 \\ & 4.1 \\ & \hline \end{aligned}$ | MHz <br> kHz <br> MHz |

ELECTRICAL CHARACTERISTICS The e indicates specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. $\mathrm{V}_{I N}=2.5 \mathrm{~V}, \mathrm{~V}_{\overline{\text { SHON }}}=2.5 \mathrm{~V}$.

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :--- | :--- | :---: | :---: | :---: | :---: |
| Maximum Switch Duty Cycle | $\mathrm{R}_{\mathrm{T}}=17.8 \mathrm{~K}$ | $\bullet$ | 84 | 93 |  |
| $\overline{\text { SHDN }}$ Pin Current | $\mathrm{V} \overline{\text { SHDN }}=5 \mathrm{~V}$ | 30 | 60 | $\mu \mathrm{~A}$ |  |
|  | $\mathrm{~V} \overline{\text { SHDN }}=0 \mathrm{~V}$ |  | 0.1 | 1 | $\mu \mathrm{~A}$ |
| $\overline{\text { SHDN }}$ Pin Threshold |  | 0.3 | 1.5 | 2 | V |
| Inductor Current Limit | $($ Note 3) | 3.5 | 5 | 6.5 | A |
| Switch Current Limit | (Note 3) | 3 | 4.5 | 6 | A |
| Switch VCESAT | ISW $=1 \mathrm{~A}($ Note 3) |  | 120 | 200 | mV |
| Switch Leakage Current | SW $=40 \mathrm{~V}$ | 0.2 | 5 | $\mu \mathrm{~A}$ |  |

Note 1: Absolute Maximum Ratings are those values beyond which the life to the device may be impaired.
Note 2: The LT3479 is guaranteed to meet performance specifications from $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$. Specifications over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ operating
temperature range are assured by design, characterization and correlation with statistical process controls.
Note 3: Inductor Current Limit, Switch Current Limit and Switch $V_{\text {CESAT }}$ for DE package guaranteed by design and/or correlation to static test.

## TYPICAL PGRFORMANCE CHARACTGRISTICS



## TYPICAL PGRFORMANCE CHARACTERISTICS



## PIn functions (denissop)

SW (Pins 1, 2/Pins 1, 2): Switch Pins. Collector of the internal NPN power switch. Connect the inductor and diode here and minimize the metal trace area connected to this pin to minimize electromagnetic interference.
L (Pin 3/Pin 3): Inductor Pin. Connect the inductor to this pin.

V (Pin 4/Pin 4): Inductor Supply. Must be locally bypassed. Powers the switch and the inductor. In case only one supply voltage is available, tie $\mathrm{V}_{\text {IN }}$ and $\mathrm{V}_{\mathrm{S}}$ together.
$V_{\text {IN }}$ (Pin 5/Pin 5): Input Supply. Must be locally bypassed. Powers the internal control circuitry.
$\mathbf{R}_{\boldsymbol{\top}}$ (Pin 6/Pin 6): Timing Resistor Pin. Adjusts the switching frequency. Do not leave this pin open. See Table 4 for $\mathrm{R}_{\top}$ values and switching frequencies.
SHDN (Pin 7/Pin 7): Shutdown. Tie to 1.5 V or greater to enable the device. Tie below 0.3 V to turn off the device.
$\mathbf{V}_{\text {REF }}$ (Pin 8/Pin 9): Bandgap Voltage Reference. Internally set to 1.235 V . Connect this pin to FBP if generating a positive output, or to an external resistor divider if generating a negative voltage. This pin can provide up to $100 \mu \mathrm{~A}$ of current and can be locally bypassed with a 100pF capacitor.

FBP (Pin 9/Pin 10): The Noninverting Input to the Error Amplifier. Connect resistive divider tap here for negative output voltage.
FBN (Pin 10/Pin 11): The Inverting Input to the Error Amplifier. Connect resistive divider tap here for positive output voltage.
$V_{\text {C }}$ (Pin 11/Pin 12): Compensation Pin for Error Amplifier. Connect a series RC from this pin to GND. Typical values are $10 \mathrm{k} \Omega$ and 2.2 nF .

SS (Pin 12/Pin 13): Soft-Start. Place a soft-start capacitor here. Leave floating if not in use.

GND (Pins 13, 14/Pins 8, 14, 15, 16): Ground. Tie directly to local ground plane.
Exposed Pad (Pin 15/Pin 17): Power Ground. Must be connected to electrical PCB ground.

## BLOCK DIAGRAM



## OPERATION

The LT3479 uses a fixed frequency, current mode control scheme to provide excellent line and load regulation. Operation can be best understood by referring to the Block Diagram. The start of each oscillator cycle sets the SR latch and turns on power switch Q1. The signal at the inverting input of the PWM comparator (SLOPE) is proportional to the sum of the switch current and oscillator ramp. When SLOPE exceeds $\mathrm{V}_{\mathrm{C}}$ (the output of the feedback amplifier), the PWM comparator resets the latch and turns off the power switch. In this manner, the feedback amplifier and PWM comparators set the correct peak current level to keep the output in regulation.
The LT3479 also features a soft-start function. During start-up, $10 \mu \mathrm{~A}$ of current charges the external soft-start capacitor. The SS pin directly limits the rate of voltage rise
on the $V_{C}$ pin, which in turn limits the peak switch current. The switch current is constantly monitored and not allowed to exceed the nominal value of 3 A . If the switch current reaches 3 A , the SR latch is reset regardless of the output of the PWM comparator. Current limit protects the power switch and external components.
In addition to soft-start, inrush current protection protects the LT3479 againstshorts and line transients. During such faults, the inductor current can momentarily exceed 3 A and damage the switch. Through an internal $8.5 \mathrm{~m} \Omega$ resistor placed in series with the inductor, the inrush current protection comparator measures the inductor current. If it exceeds 5 A , a soft-start cycle is initiated. The LT3479 will remain in the soft-startcondition until the fault has passed.

## APPLICATIONS InFORMATION

## Capacitor Selection

Low ESR (equivalent series resistance) ceramic capacitors should be used at the output to minimize the output ripple voltage. Use only X5R or X7R dielectrics, as these materials retain their capacitance over wider voltage and temperature ranges better than other dielectrics. A $4.7 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$ output capacitor is sufficient for most high output current designs. Converters with lower output currents may need only a $1 \mu \mathrm{~F}$ or $2.2 \mu \mathrm{~F}$ output capacitor.
Table 1. Ceramic Capacitor Manufacturers

| MANUFACTURER | PHONE | WEB |
| :--- | :--- | :--- |
| Taiyo Yuden | $(408) 573-4150$ | www.t-yuden.com |
| AVX | $(803) 448-9411$ | www.avxcorp.com |
| Murata | $(714) 852-2001$ | www.murata.com |

## Inductor Selection

Several inductors that work well with the LT3479 are listed in Table 2. However, there are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and their entire range of parts. Ferrite core inductors should be used to obtain the best efficiency. Choose an inductor that can handle the necessary peak current without saturating, and ensure that the inductor has a low DCR (copper-wire resistance) to minimize $I^{2}$ R power losses. A $4.7 \mu \mathrm{H}$ or $10 \mu \mathrm{H}$ inductor will suffice for most LT3479 applications.
Inductor manufacturers specify the maximum current rating as the current where the inductance falls to some percentage of its nominal value-typically $65 \%$. An
inductor can pass a current larger than its rated value without damaging it. Aggressive designs where board space is precious will exceed the maximum current rating of the inductor to save board space. Consult each manufacturer to determine how the maximum inductor current is measured and how much more current the inductor can reliably conduct.

Physically larger inductors provide better efficiency than smaller ones. Figure 1 shows a 3\% to 4\% efficiency gain in using a larger inductor in a $1 \mathrm{MHz}, 5 \mathrm{~V}$ to 12 V application. The efficiency of the TOKO FDV0630-4R7M, which measures $7 \mathrm{~mm} \times 7.7 \mathrm{~mm}$ and 3 mm thick, peaks at $87 \%$. The smaller Sumida CDRH4D28-4R7 which is $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ and 3 mm thick yields a peak efficiency of $85 \%$ in an identical application. Thus, if board space is abundant, then larger inductors should be used to maximize efficiency.


Figure 1. Efficiency vs Inductor Size

Table 2. Suggested Inductors

| MANUFACTURER <br> PART NUMBER | IDC <br> $(\mathbf{A})$ | INDUCTANCE <br> $(\boldsymbol{\mu} \mathbf{)})$ | MAX DCR <br> $(\mathbf{m} \Omega)$ | $\mathbf{L} \times \mathbf{W} \times \mathbf{H}$ <br> $(\mathbf{m m})$ | MANUFACTURER |
| :--- | :---: | :---: | :---: | :---: | :--- |
| CDRH6D283R0 | 3 | 3 | 24 | $6.7 \times 6.7 \times 3.0$ | Sumida |
| CDRH6D28100 | 1.7 | 10 | 65 | $6.7 \times 6.7 \times 3.0$ | www.sumida.com |
| CDRH4D284R7 | 1.32 | 4.7 | 72 | $5.0 \times 5.0 \times 3.0$ |  |
| LM N 05D B4R7M | 2.2 | 4.7 | 49 | $5.9 \times 6.1 \times 2.8$ | Taiyo Yuden |
| LM N 05D B100K | 1.6 | 10 | 10 | $5.9 \times 6.1 \times 2.8$ | www.t-yuden.com |
| LQH55DN4R7M01L | 2.7 | 4.7 | 57 | $5.7 \times 5.0 \times 4.7$ | Murata |
| LQH55DN100M01K | 1.7 | 10 | 130 | $5.7 \times 5.0 \times 4.7$ | www.murata.com |
| FDV0630-4R7M | 4.2 | 4.7 | 49 | $7.0 \times 7.7 \times 3.0$ | Toko |
|  |  |  |  |  | www.toko.com |

## APPLICATIONS INFORMATION

## Diode Selection

Schottky diodes, with their low forward voltage drop and fast switching speed, are ideal for LT3479 applications. Table 3 lists several Schottky diodes that work well with the LT3479. The diode's average current rating must exceed the average output current. The diode's maximum reverse voltage must exceed the output voltage. The diode conducts current only when the power switch is turned off (typically less than $50 \%$ duty cycle), so a 3 A diode is sufficient for most designs. The companies below also offer Schottky diodes with high voltage and current ratings.
Table 3. Suggested Diodes

| MANUFACTURER <br> PART NUMBER | MAX <br> CURRENT (A) | MAX REVERSE <br> VOLTAGE (V) | MANUFACTURER |
| :--- | :---: | :---: | :--- |
| UPS340 | 3 | 40 | Microsemi |
| UPS315 | 3 | 15 | www.microsemi.com |
| B220 | 2 | 20 | Diodes, Inc |
| B230 | 2 | 30 | www.diodes.com |
| B240 | 2 | 40 |  |
| B320 | 3 | 20 |  |
| B330 | 3 | 30 |  |
| B340 | 3 | 40 |  |
| SBM340 | 3 | 40 |  |

## Setting Positive Output Voltages

To set a positive output voltage, select the values of R1 and R2 (see Figure 2) according to the following equation:

$$
\mathrm{V}_{\text {OUT }}=1.235 \mathrm{~V}\left(1+\frac{\mathrm{R} 1}{\mathrm{R} 2}\right)
$$



Figure 2. Positive Output Voltage Feedback Connections

## Setting Negative Output Voltages

To set a negative output voltage, select the values of R3 and R4 (see Figure 3) according to the following equation:

$$
\mathrm{V}_{\text {OUT }}=-1.235 \mathrm{~V}\left(\frac{\mathrm{R} 3}{\mathrm{R} 4}\right)
$$



Figure 3. Negative Output Voltage Feedback Connections

## Board Layout

As with all switching regulators, careful attention must be paid to the PCB board layout and component placement. To maximize efficiency, switch rise and fall times are made as short as possible. To prevent radiation and high frequency resonance problems, proper layout of the high frequency switching path is essential. Minimize the length and area of all traces connected to the SW pin and always use a ground plane under the switching regulator to minimize interplane coupling. The signal path including the switch, output diode D1 and output capacitor $\mathrm{C}_{0 \mathrm{U}}$, contains nanosecond rise and fall times and should be kept as short as possible. Recommended component placement is shown in Figure 4.

## Soft-Start

For many applications, it is necessary to minimize the inrush current at start-up. The built-in soft-start circuit significantly reduces the start-up current spike and output voltage overshoot. A typical value is 10 nF for 1.65 ms . Figure 5 shows the start-up output voltage and inductor current waveforms in a typical application without a softstart capacitor. Notice the output voltage overshoot and the large initial current. The addition of a 22 nF capacitor eliminates the output overshoot and reduces the peak inductor current (Figure 6).

## APPLICATIONS InFORMATION



Figure 4. Suggested Board Layout


Figure 5. Start-Up with No Soft-Start Capacitor

$0.2 \mathrm{~ms} / \mathrm{DIV}$

Switching Frequency
The switching frequency of the LT3479 is set by an external resistor attached to the RT pin. Do not leave this pin open. A resistor must always be connected for proper operation. See Table 4 and Figure 7 for resistor values and corresponding frequencies.
Table 4. Switching Frequency

| SWITCHING FREQUENCY (MHz) | $\mathbf{R}_{\boldsymbol{T}} \mathbf{( k \Omega )}$ |
| :---: | :---: |
| 3.5 | 1.78 |
| 3 | 2.87 |
| 2.5 | 4.32 |
| 2 | 6.49 |
| 1.5 | 10.2 |
| 1 | 17.8 |
| 0.5 | 39.2 |
| 0.2 | 113 |

Figure 6. Start-Up with Css $=22 n F$

## APPLICATIONS IIFORMATION

Increasing switching frequency reduces output voltage ripple but also reduces efficiency. The user should set the frequency for the maximum tolerable output voltage ripple. Figure 8 shows a reduction in efficiency of about 4\% between 1 MHz and 2 MHz operation.

## Inrush Current Protection

The LT3479 features a novel inductor current sensing circuit that protects the LT3479 during hot plugging and short circuits. An internal resistor in series with the


Figure 7. Switch Frequency


Figure 8. Efficiency vs Switching Frequency
external inductor senses the inductor current at all times. When it exceeds 5A, a soft-start cycle is initiated. Figure 9 shows an output short circuit with inrush current protection disabled. Notice that soft-start remains high, and that the inductor current does not return to zero. Figure 10 illustrates the benefits of inrush current protection. The output short initiates a new soft start cycle reducing the inductor current. After the fault has passed, the inductor current slowly returns to its equilibrium value.
Bypassing the $8.5 \mathrm{~m} \Omega$ inductor current sense resistor disables inrush current protection. Connect the inductor supply trace and bypass capacitor to the L pin and leave the $V_{S}$ pin open to disable this feature.


Figure 9. Output Short with Inrush Current Protection Enabled


Figure 10. Output Short with Inrush Current Protection Disabled


Figure 11

## TYPICAL APPLICATIONS

## 800mA, 5V to 12V Boost Converter




3479 tA03b

500kHz, 800 mA , 5 V to 12 V Boost Converter


## TYPICAL APPLICATIONS

900mA, 3.3V to 8V Boost Converter



3479 TA05b

5V to -5V, 600mA Inverting DC/DC Converter



## TYPICAL APPLICATIONS

83\% Efficient, 5W Lumileds Luxeon ${ }^{\text {TM }}$ Driver


## TYPICAL APPLICATIONS

500mA, 12 White LED Driver


Efficiency


3479 TA08b

## DE Package

14-Lead Plastic DFN ( $4 \mathrm{~mm} \times 3 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1708)


RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS


NOTE:

1. DRAWING PROPOSED TO BE MADE VARIATION OF VERSION (WGED-3) IN JEDEC PACKAGE OUTLINE MO-229
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

PACKAGE DESCRIPTION
FE Package
16-Lead Plastic TSSOP (4.4mm)
(Reference LTC DWG \# 05-08-1663)
Exposed Pad Variation BC


RECOMMENDED SOLDER PAD LAYOUT


NOTE:

1. CONTROLLING DIMENSION: MILLIMETERS
2. DIMENSIONS ARE IN $\frac{\text { MILLIMETERS }}{\text { (INCHES) }}$
3. DRAWING NOT TO SCALE

4. RECOMMENDED MINIMUM PCB METAL SIZE

FOR EXPOSED PAD ATTACHMENT
*DIMENSIONS DO NOT INCLUDE MOLD FLASH. MOLD FLASH
SHALL NOT EXCEED 0.150 mm (.006") PER SIDE

## TYPICAL APPLICATION

Lumiled Driver for Photo Flash with Output Disconnnect


## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT1618 | Constant Current, Constant Voltage 1.4MHz, High Efficiency Boost Regulator | $\mathrm{V}_{\text {IN }}$ : 1.6 V to $18 \mathrm{~V}, \mathrm{~V}_{\text {OUt(MAX) }}=5.5 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}=2.5 \mathrm{~mA}, \mathrm{I}_{\text {SD }}=<1 \mathrm{HA}, \mathrm{QFN} 16$ Package |
| LTC ${ }^{\text {® }} 3216$ | 1A Low Noise High Current LED Charge Pump with Independent Torch/Flash Current Control | $\mathrm{V}_{\text {IN: }}: 2.9 \mathrm{~V}$ to 4.4V, $\mathrm{V}_{\text {OUt(MAX }}=5.5 \mathrm{~V}, \mathrm{I}_{\mathrm{O}}=300 \mu \mathrm{~A}, \mathrm{I}_{\text {SD }}=<1 \mu \mathrm{~A}$, DFN12 Package |
| LTC3436 | 3 A (Isw), 1MHz, 34V Step-Up DC/DC Converter | $\mathrm{V}_{\text {IV: }}: 3 \mathrm{~V}$ to 25V, $\mathrm{V}_{\text {OUT(MAX }}=34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}=0.9 \mathrm{~mA}, \mathrm{I}_{\text {SD }}=<6 \mu \mathrm{~A}, \mathrm{TSSOP} 16 \mathrm{P}$ Package |
| LTC3453 | Synchronous Buck-Boost High Power White LED Driver | $\mathrm{V}_{\text {IV: }}$ : 2.7 V to $5.5 \mathrm{~V}, \mathrm{~V}_{\text {OUt(MAX }}=5.5 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}=2.5 \mathrm{~mA}, \mathrm{I}_{\text {SD }}=<1 \mu \mathrm{~A}, \mathrm{QFN} 16$ Package |
| LT3466 | Dual Constant Current, 2MHz, High Efficiency White LED Boost Regulator with Integrated Schottky Diode | $\mathrm{V}_{\text {IW }}$ : 2.7 V to $24 \mathrm{~V}, \mathrm{~V}_{\text {OUt(MAX) }}=40 \mathrm{~V}, \mathrm{I}_{\text {l }}=5 \mathrm{~mA}, \mathrm{I}_{\text {SD }}=<16 \mu \mathrm{~A}$, DFN Package |


[^0]:    $\boldsymbol{\mathcal { Y }}$, LTC and LT are registered trademarks of Linear Technology Corporation.

